

**DCS cloud comparison between
MODIS/GOES and ARM surface-aircraft
measurements during MC3E at ARM SGP**

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ARM observations/retrievals during MC3E

- **Cloud top height: KAZR radar at DOE ARM SGP site;**
- **Particle size: using newly developed retrieval algorithms**

Method 1: retrieved re based on KAZR reflectivity and number concentration measured by UND Citation;

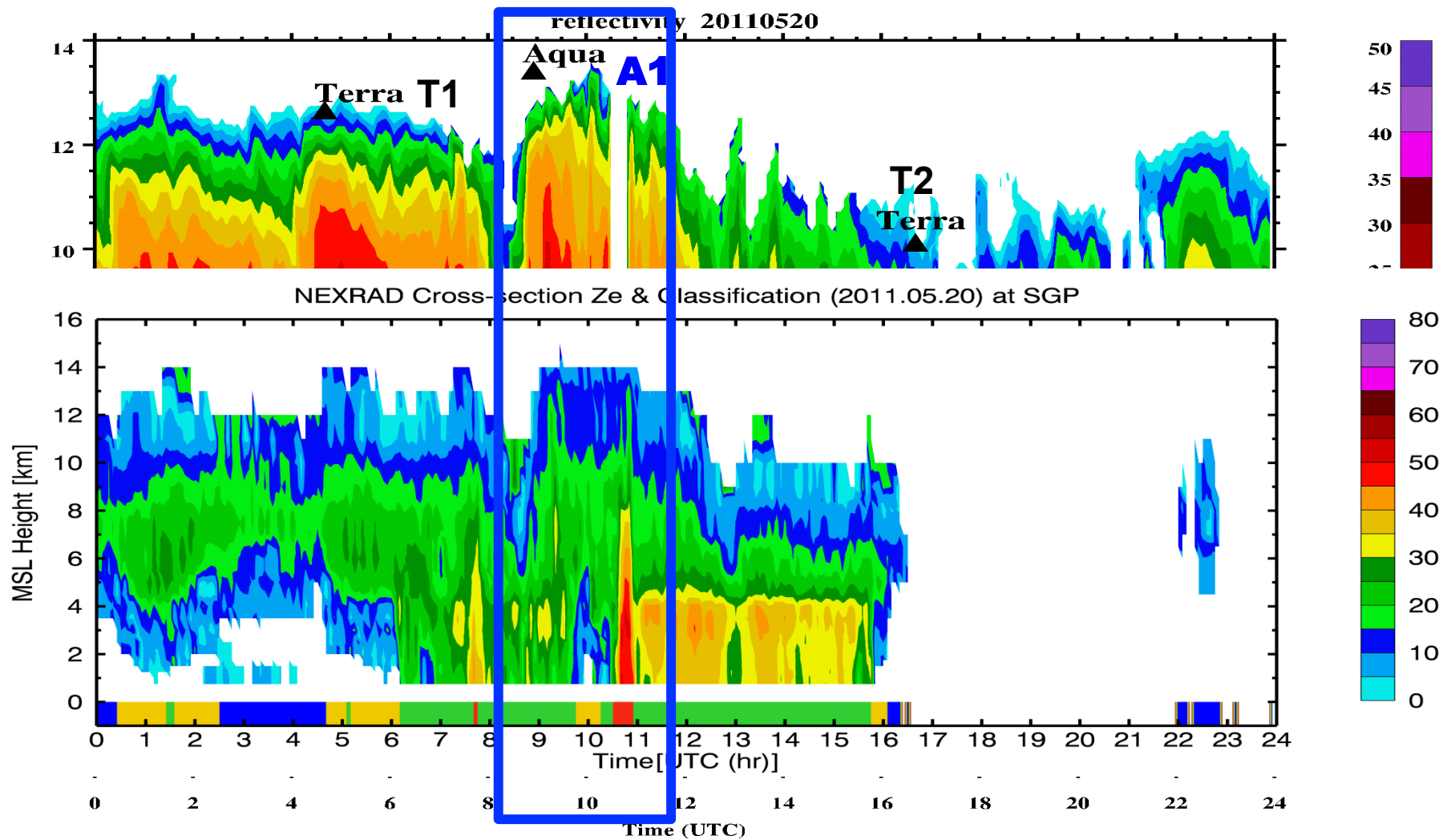
Method 2: retrieved re based on the terminal velocity;

Both are compared with UND aircraft in situ data

Cloud-top height comparison between radars and MODIS/GOES (May 20th, 2011)

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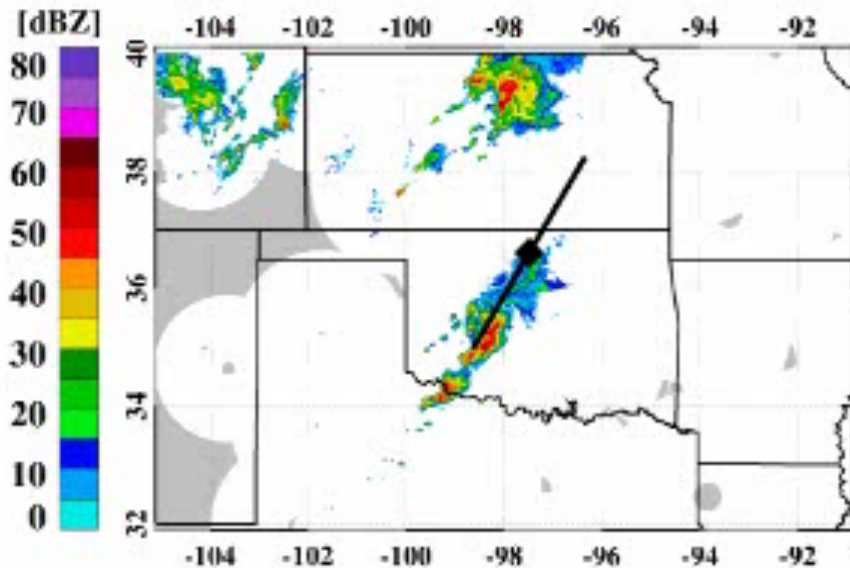


Terra MODIS heights (T1 & T2) agree with radar cloud-top heights; Z_{top} at Aqua overpass (A2) is lower than the radar measured cloud top \rightarrow This is reasonable for optically thin clouds.

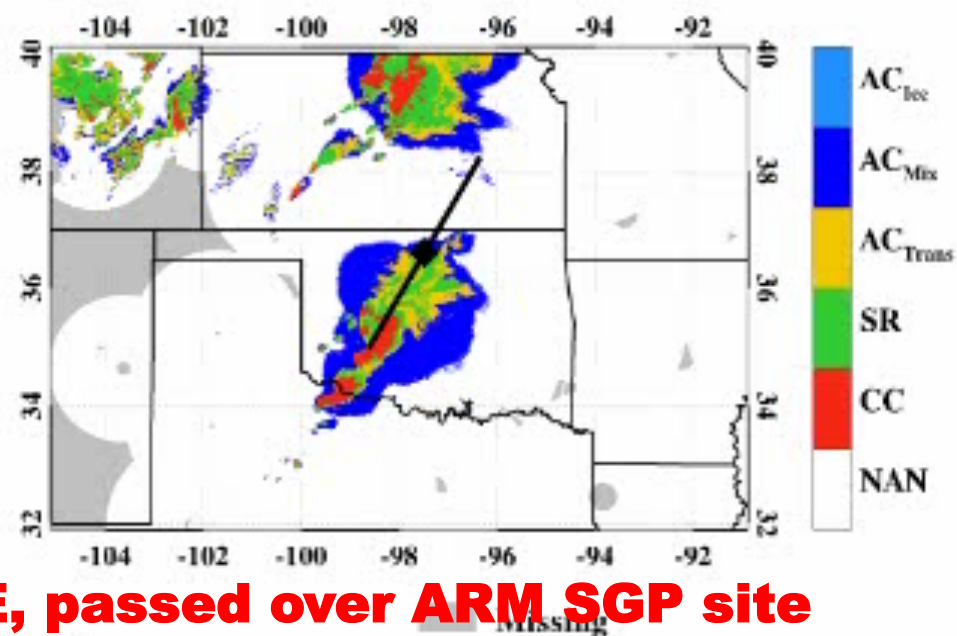
Z_{top} at A1 is ~ 1 km higher than the radar cloud top because it is surrounded by the convective core and the radar signal might be attenuated by the precipitation, but NEXRAD detected $Z_{\text{top}} \sim 14$ km.

2011.05.20 00:00 UTC

(a) 2500 m Z_e

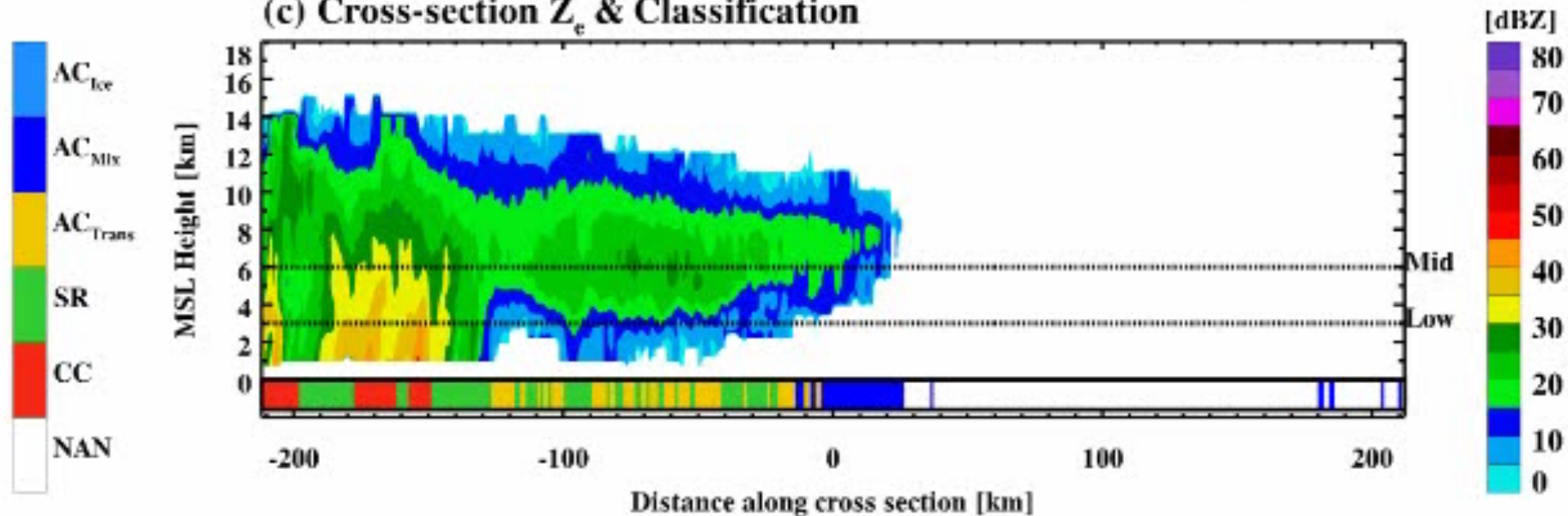


(b) Classification



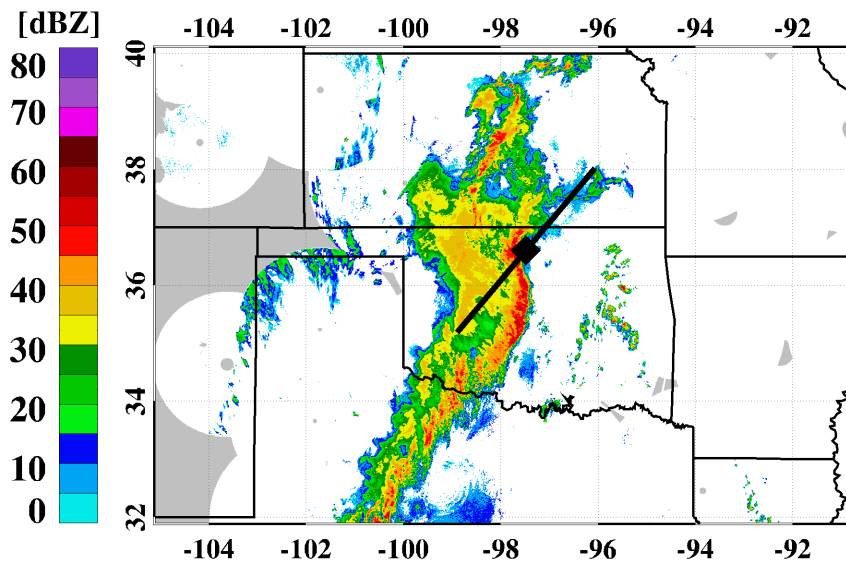
System moved from SW to NE, passed over ARM SGP site

(c) Cross-section Z_e & Classification

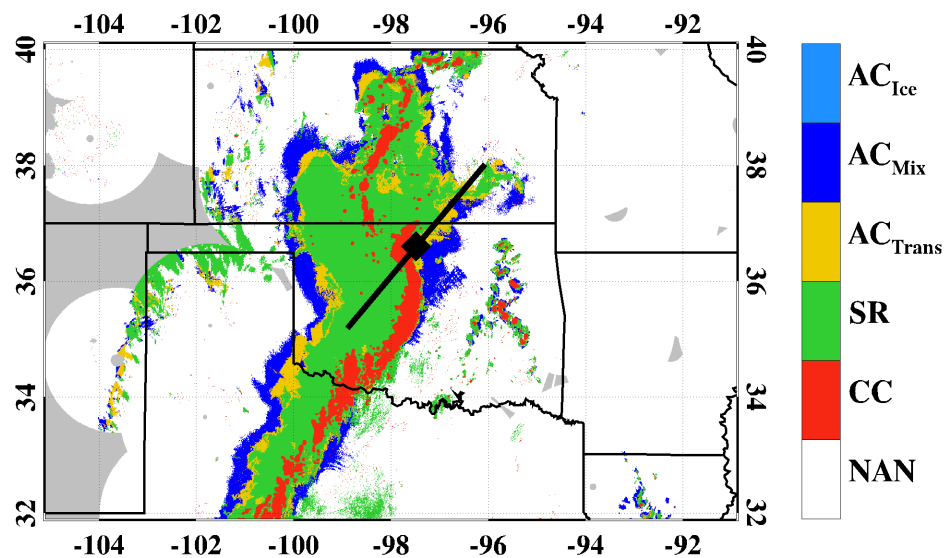


2011.05.20 10:10 UTC

(a) 2500 m Z_e

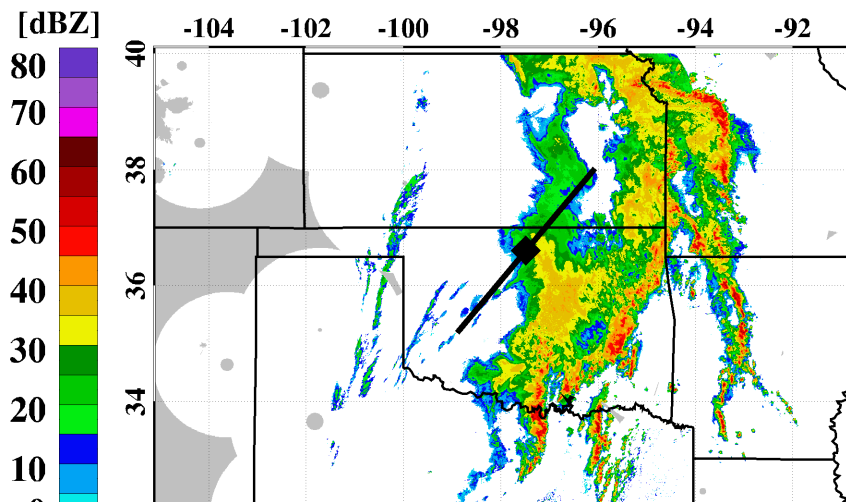


(b) Classification

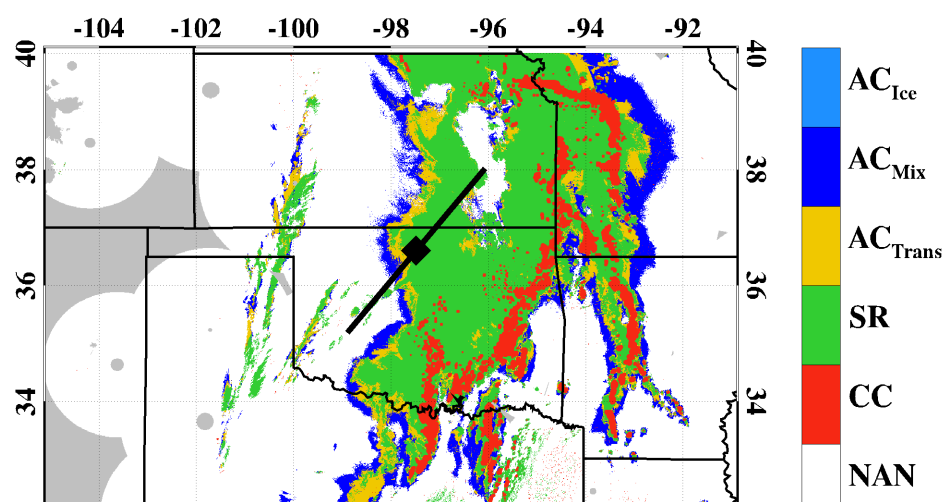


2011.05.20 15:45 UTC

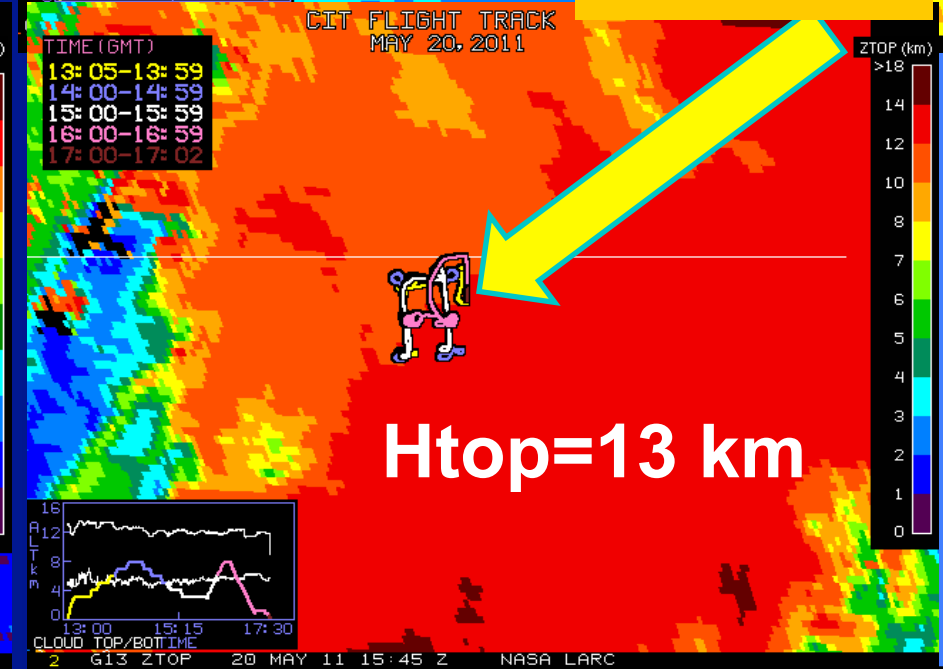
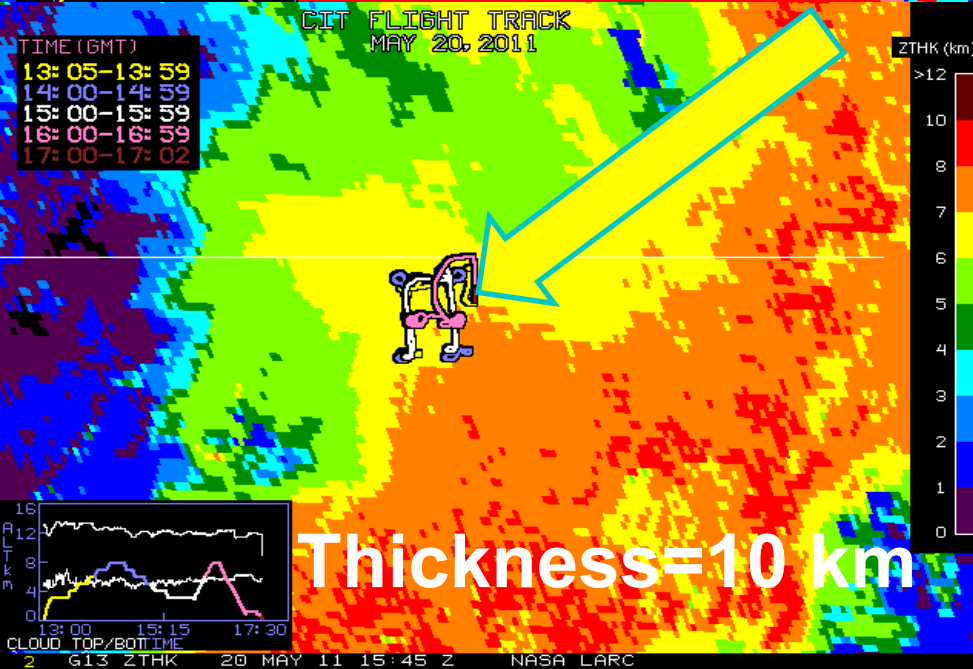
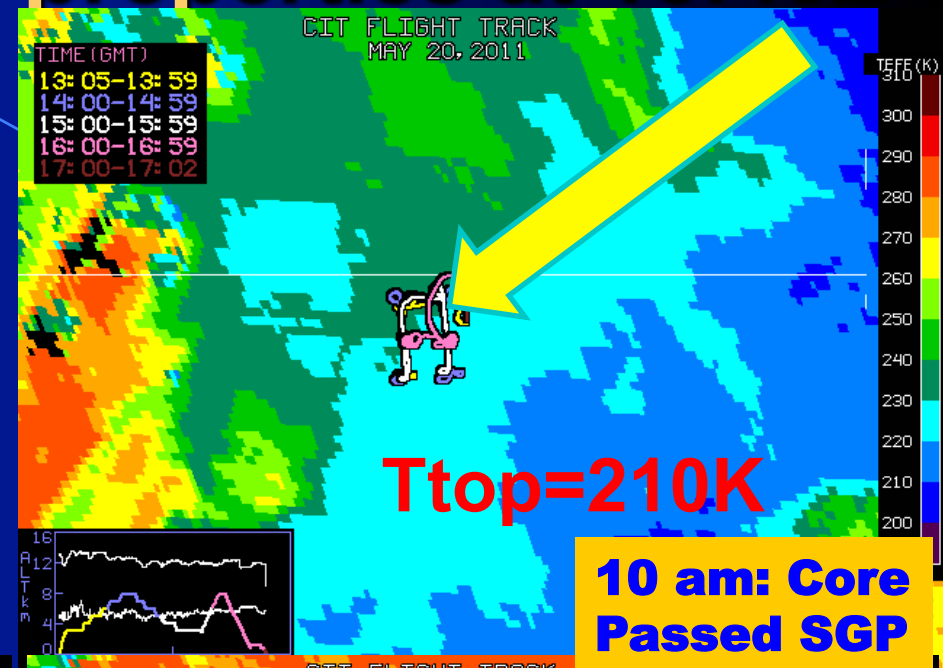
(a) 2500 m Z_e



(b) Classification



GOES retrieved cloud properties at 15:45Z



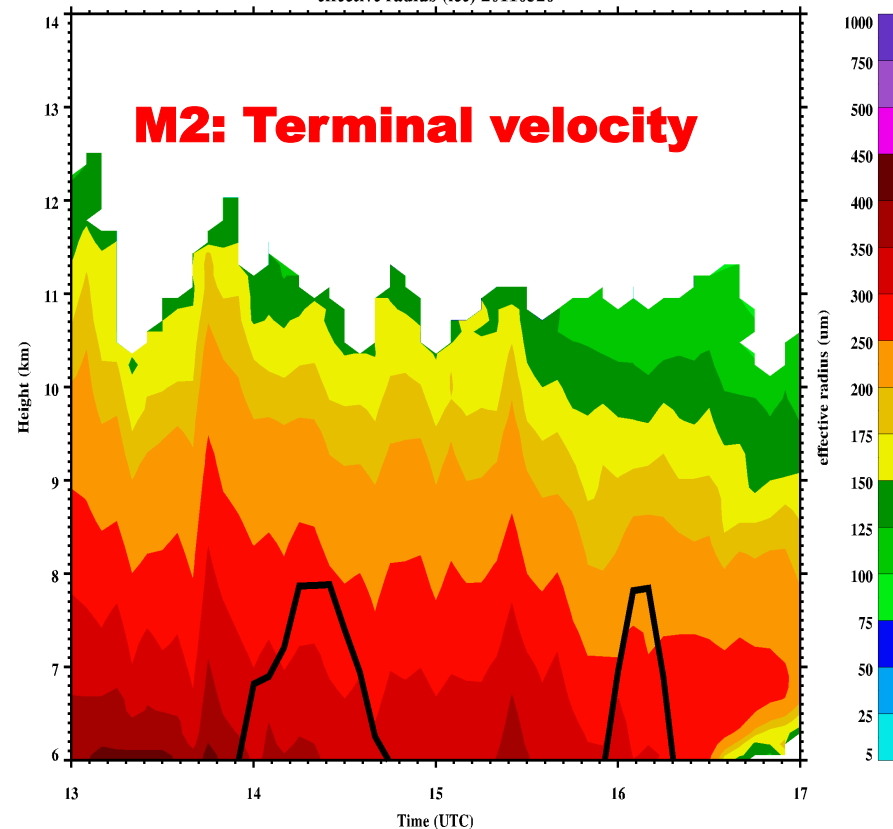
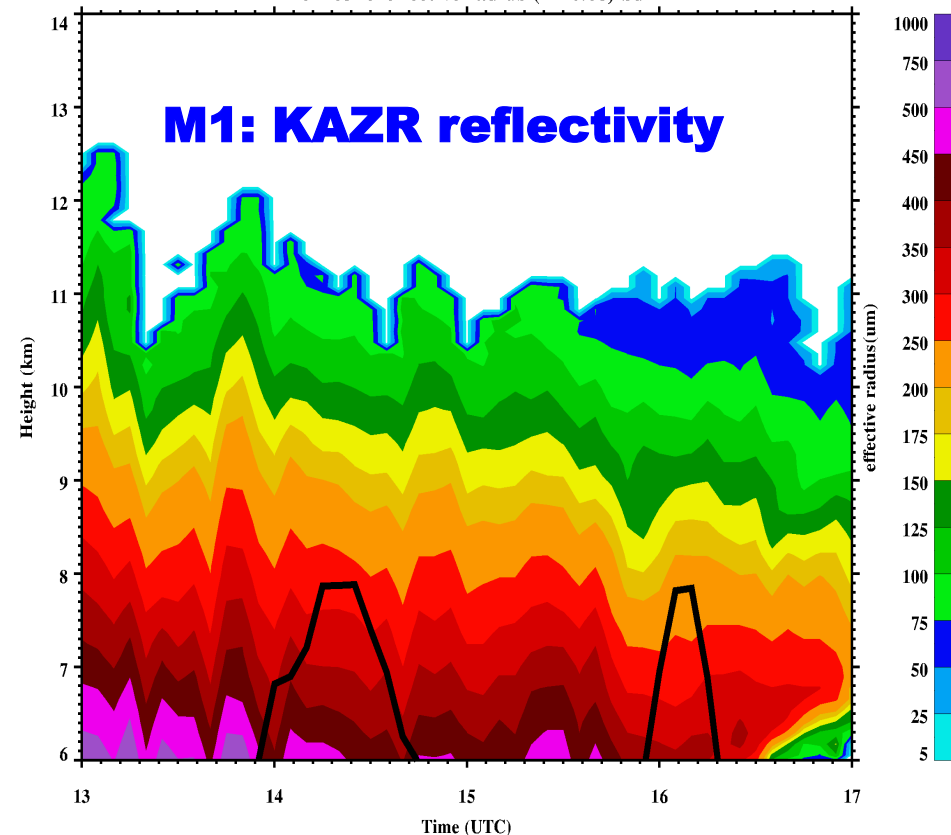
Conclusion:

Both MODIS and GOES retrieved cloud-top heights for DCS are within ARM Cloud and NEXRAD radar observations for this case.

Two new methods are developed to retrieve DCS particle size (re)

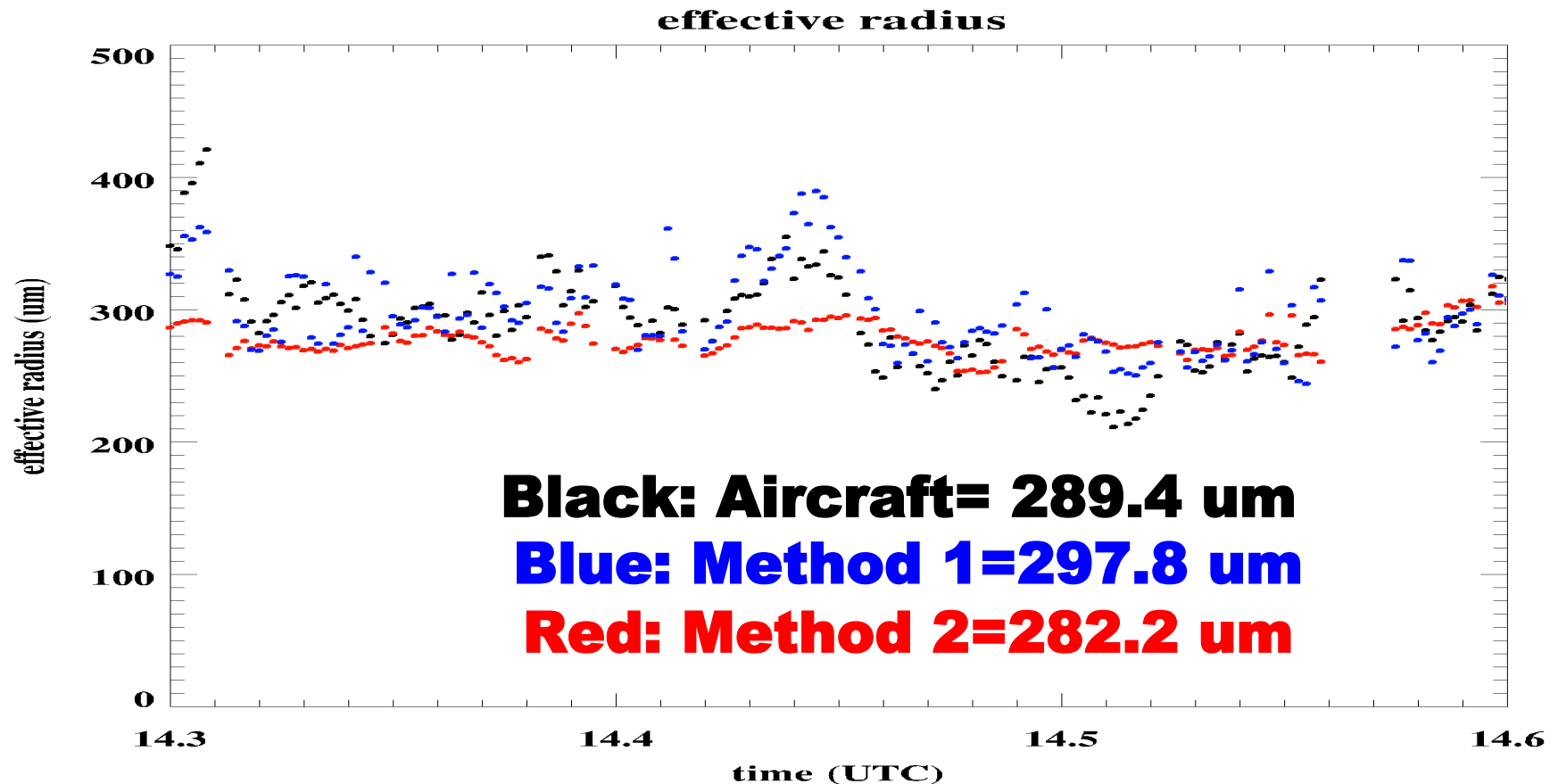
20110520 effective radius ($n=0.06$) bd

effective radius (ice) 20110520



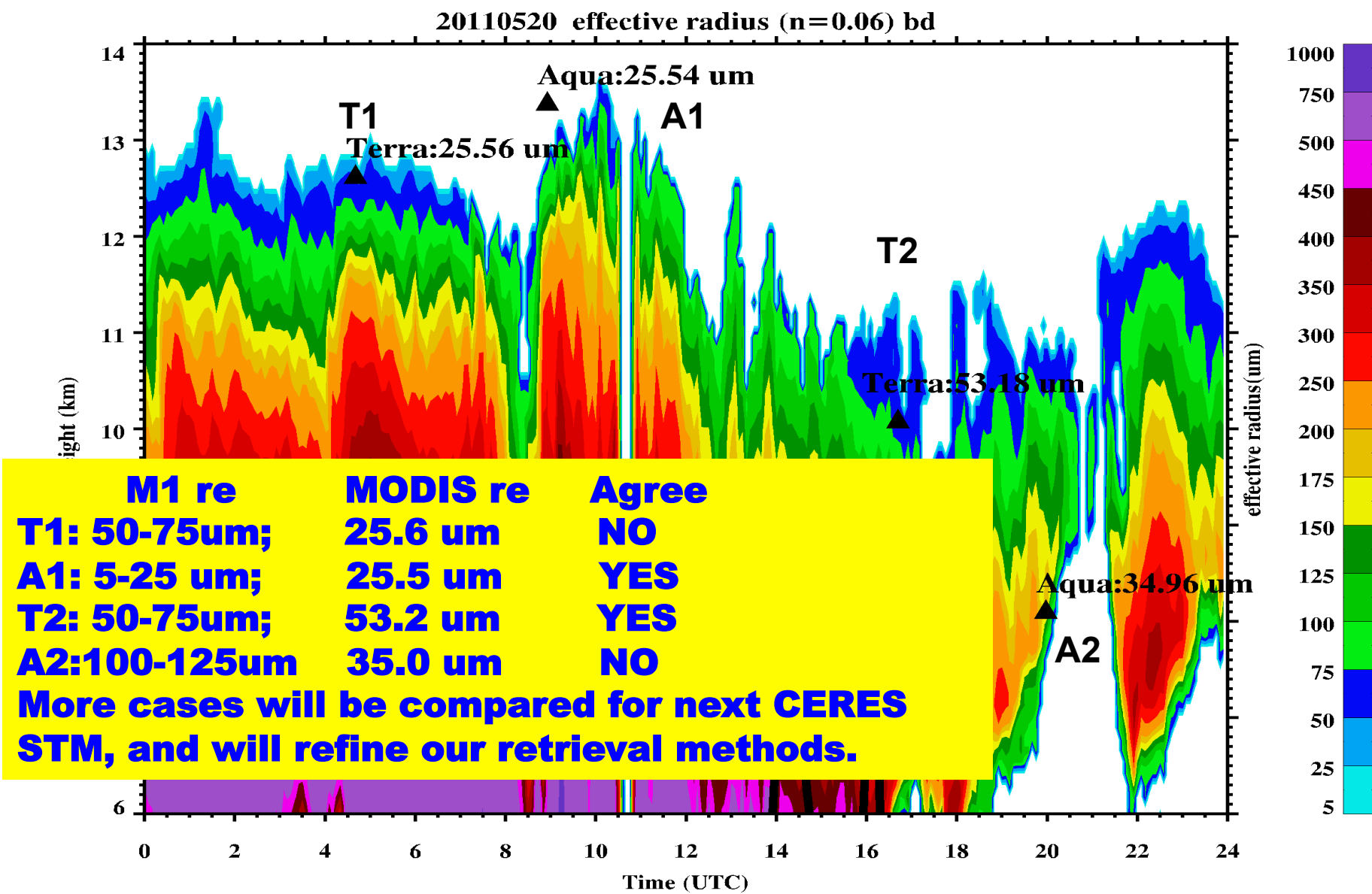
- **Black lines are aircraft flight tracks. The aircraft measurements above 6 km will be used for validating M1 and M2 ice cloud re values.**
- **M1 re values have much finer vertical resolution than those from M2.**
- **M1 re values increase from 50 um at cloud top to 300 um at 7 km, they are about 25-50 um smaller than those from M2 at upper levels.**

Validation of M1 and M2 results using aircraft data

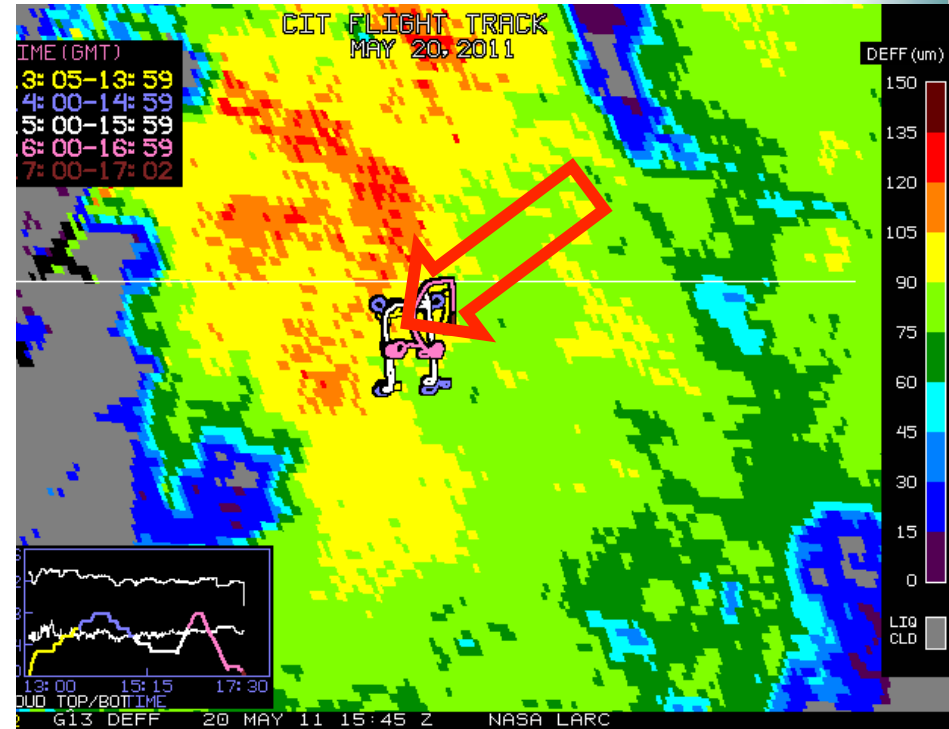
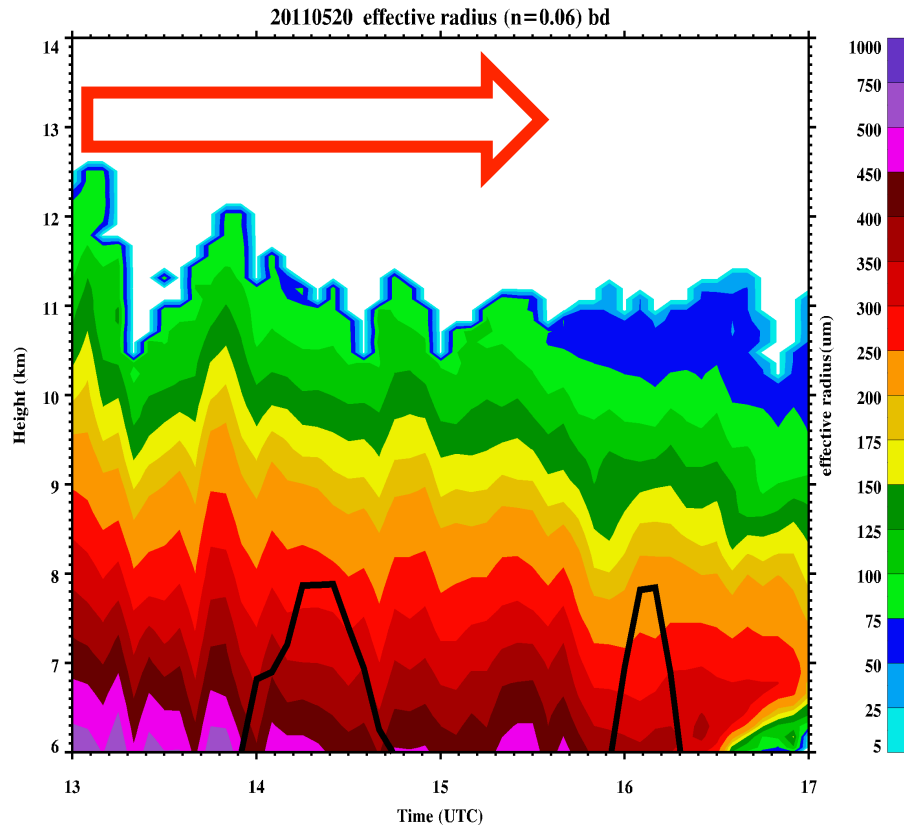


Although their means are close to each other, the correlation of **M1** retrieved re with aircraft data is **0.7**, while **M2** is **0.11**. Both methods need to be further validated by aircraft data with more cases during MC3E IOP.

Method 1: Combined KAZR reflectivity with Aircraft measured cloud number concentration

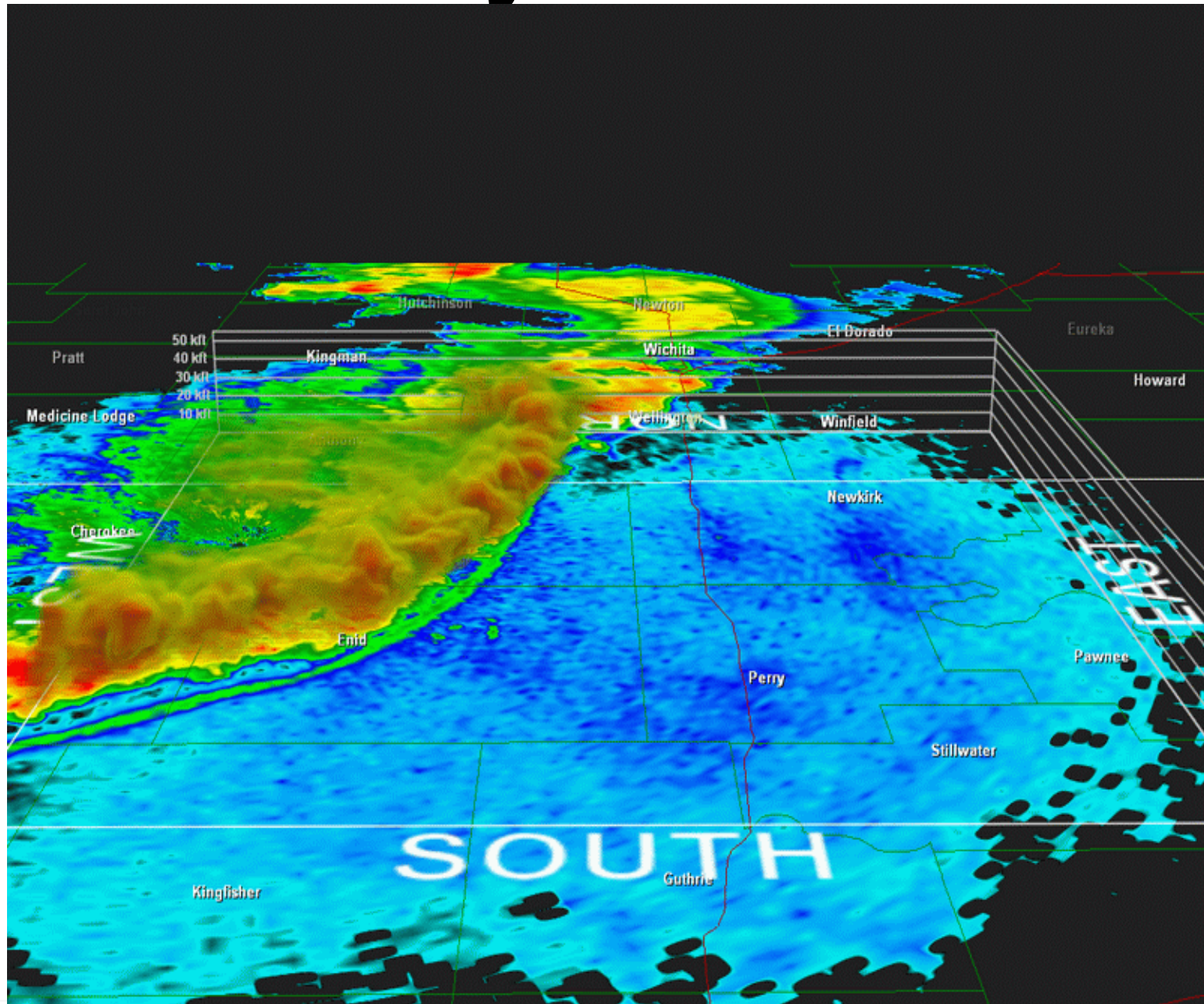


GOES retrieved cloud properties at 15:45Z



**ARM re values range from 75-125 um,
GOES De values range from 75-120 um.**

Thanks for your attention!



Parameterization of Cloud thickness vs cloud LWP and cloud-top temp

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Data

- **Data used**

- **ARM SGP Site (Oklahoma) 10 years of data (1997-2006)**
- **ARM Azores site (Atlantic) 19 months of data (2009-2010)**
- **ARM NSA site (Barrow, Alaska) 6 years of data (1999-2004)**
 - **Only use May-September data for NSA site**

- **Variables**

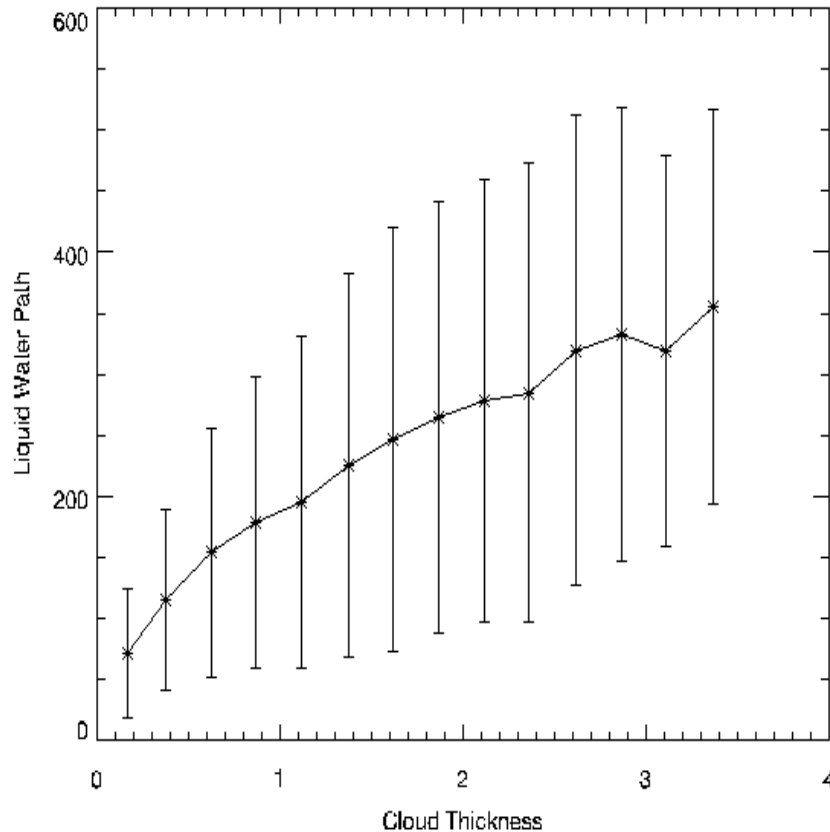
- **Liquid Water Path**
- **Cloud Thickness**
- **Cloud Top Temperature**

Methods

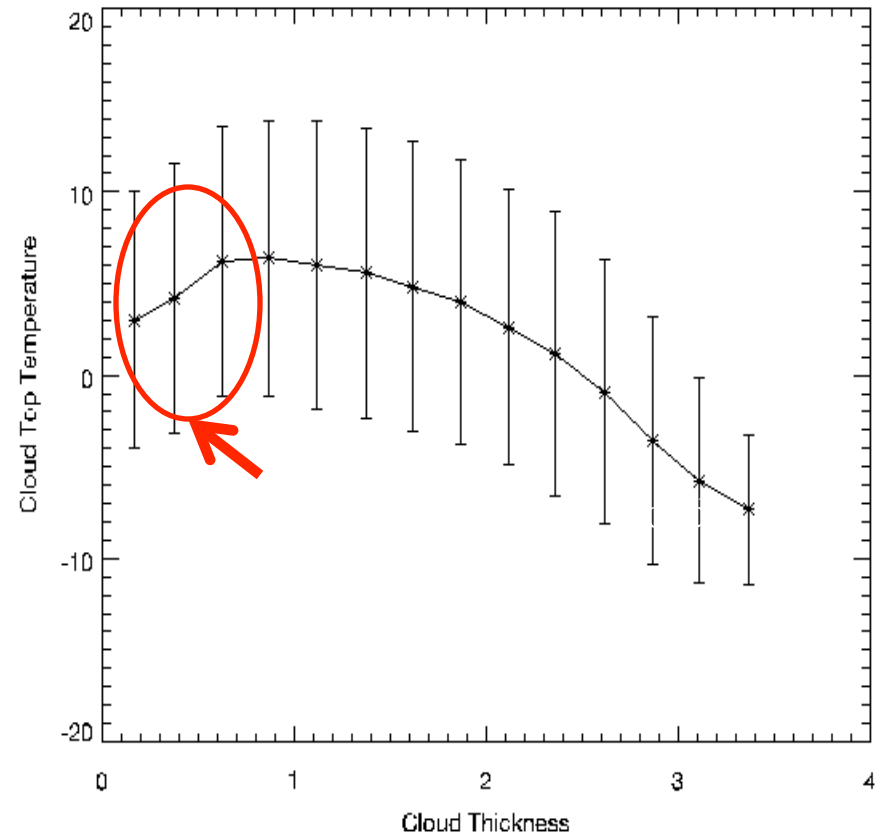
- **Cloud Top Temperature Threshold= 260K+**
- **Low Clouds (Cloud Top Height< 4km)**
- **Removed twilight hours(except NSA site)**
- **Cloud Thickness > 50 m**
- **Liquid Water Path must be between 20 and 700 g/m²**
- **Bin**
 - **Took average of all values every 250 meters of cloud thickness**
- **Multiple Linear Regression line fit**
- **Statistics**
 - **Multiple linear correlation coefficient (R-Value)**

SGP

Mean Cloud Thickness vs Mean Liquid Water Path SGP

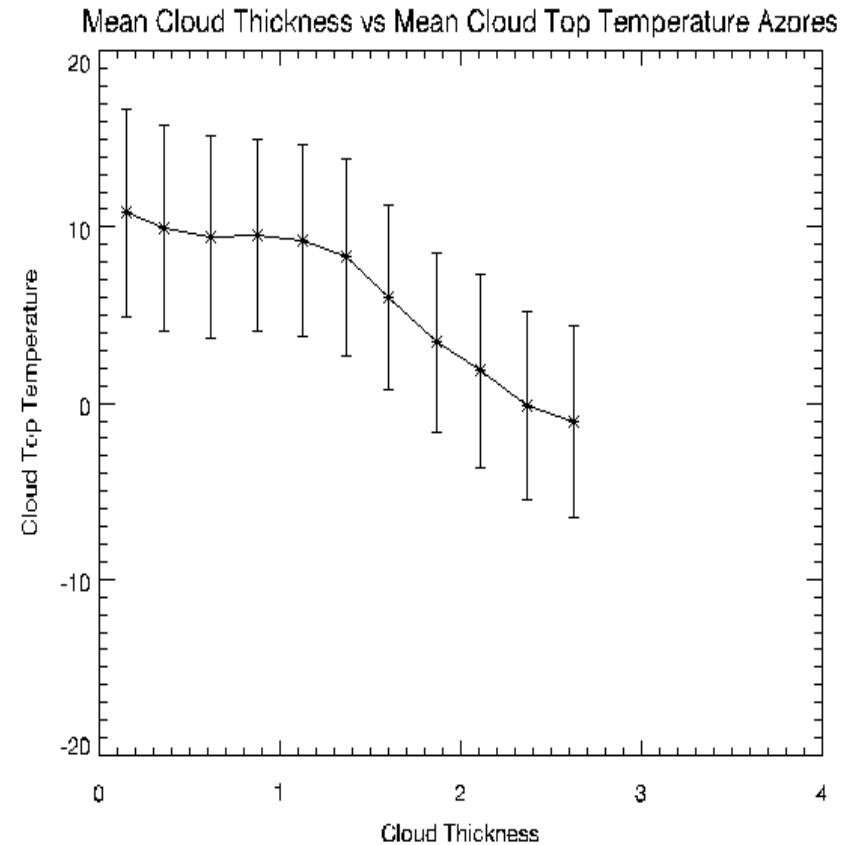
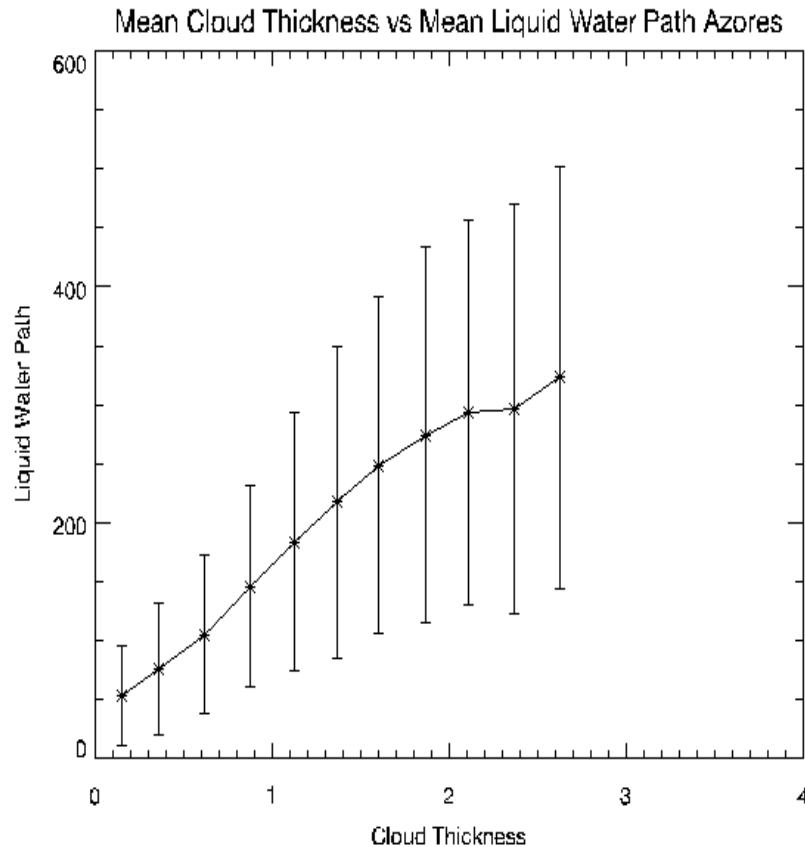


Mean Cloud Thickness vs Mean Cloud Top Temperature SGP



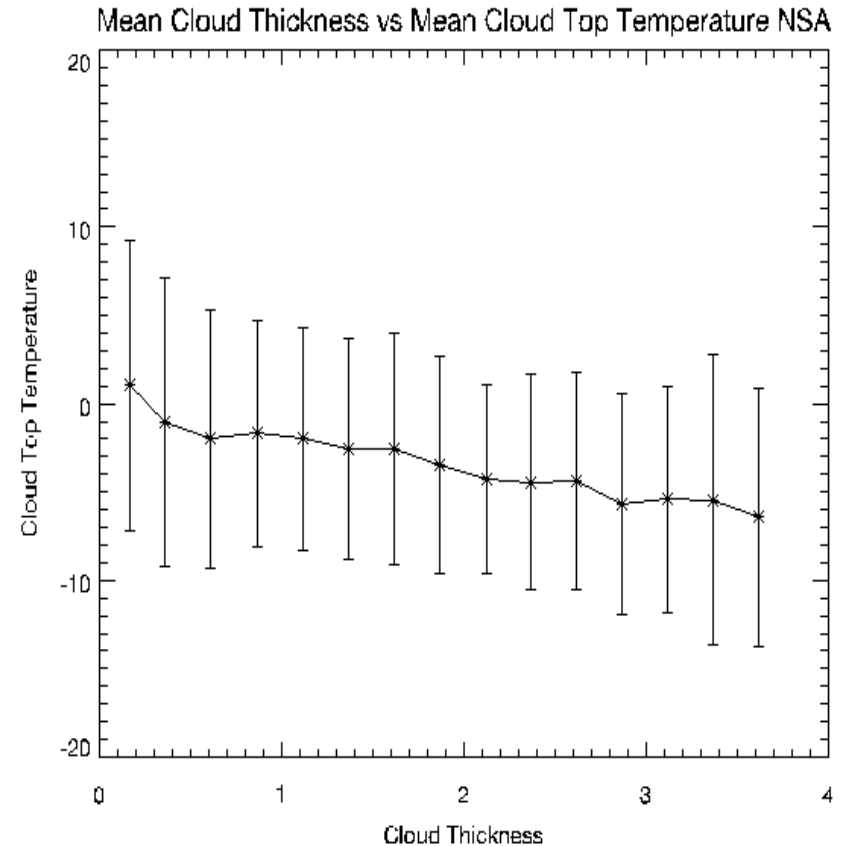
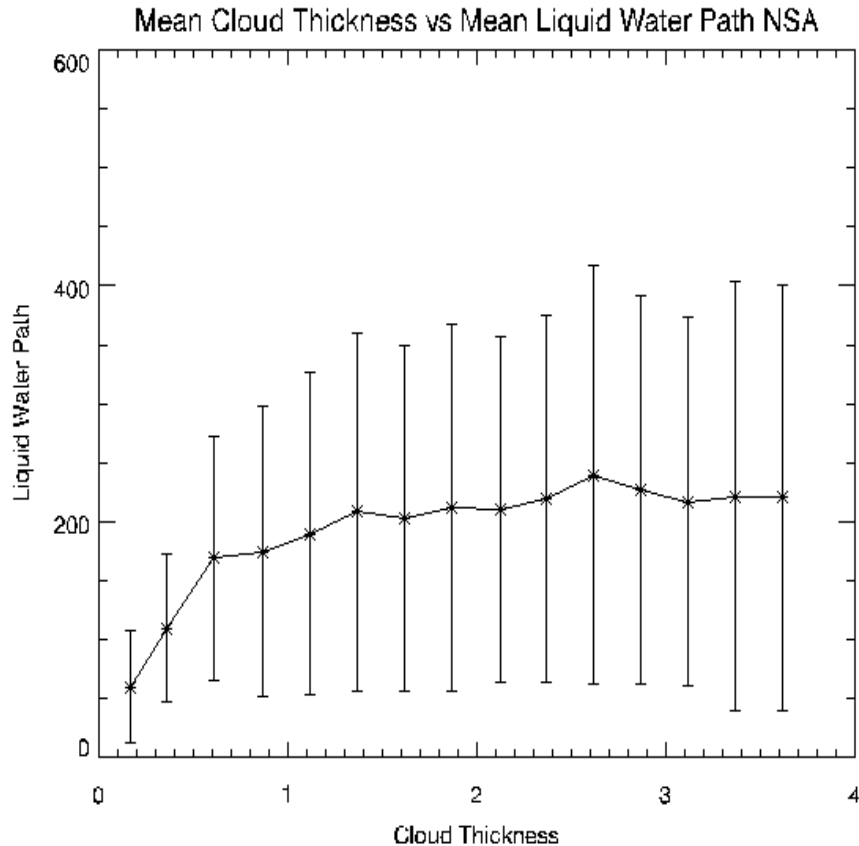
- $\Delta Z = .0021 * LWP - .004 * (T_{top} - T_0) + .588$
- **R-value=.458**

Azores



- $\Delta Z = .0029 * LWP - .037 * (T_{top} - T_0) + .784$
- R-value=.72

NSA

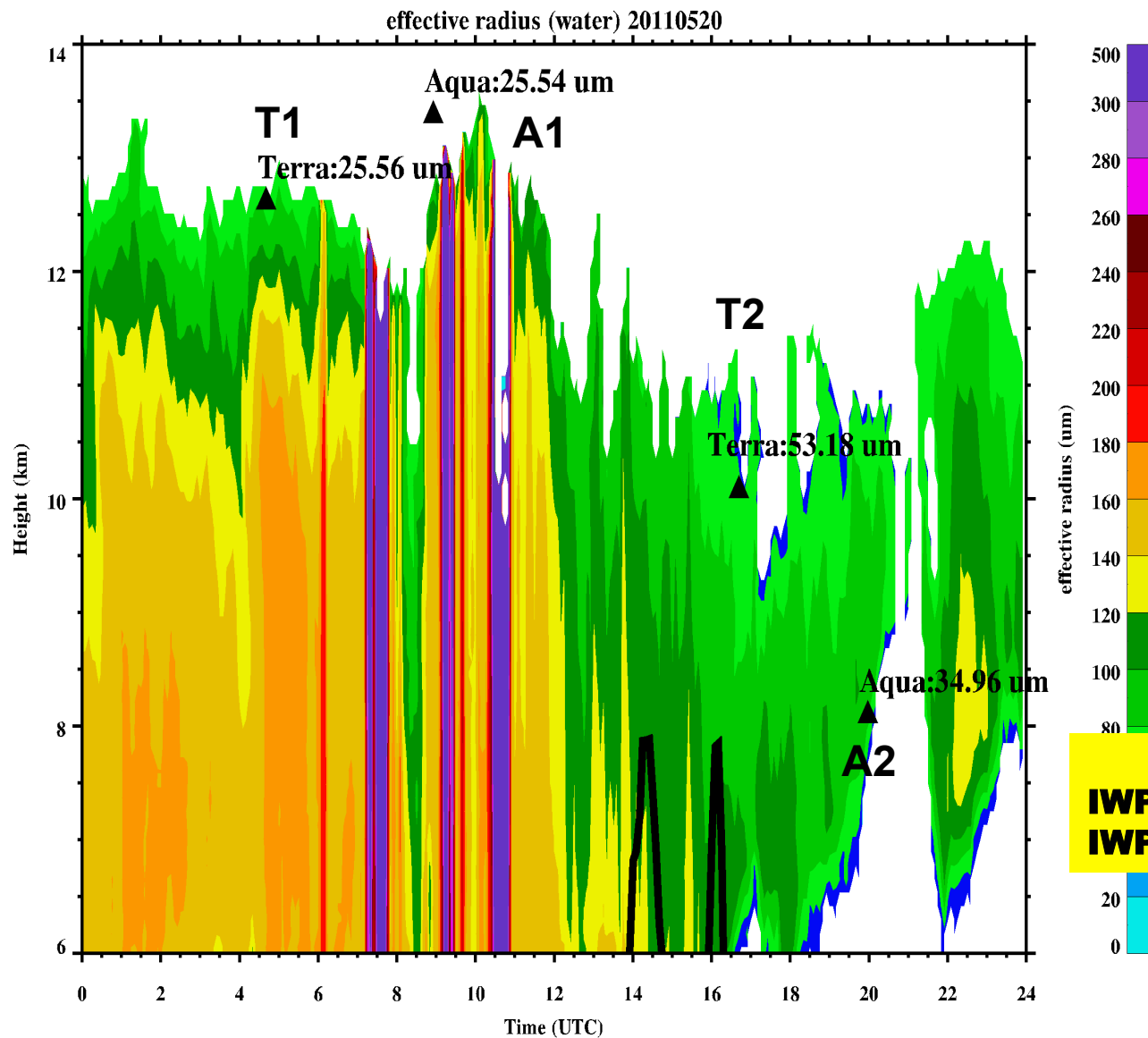


- $\Delta Z = .0025 * LWP - .015 * (T_{top} - T_0) + .359$
- **R-value=.45**

Conclusion/Future Improvements

- **Similarities between ARM sites**
 - **Linear relationship between Cloud Top temperature and Cloud Thickness**
 - **Logarithmic relationship between Liquid Water Path and Cloud Thickness**
- **Differences between ARM sites**
 - **Due to the high variability of data at the NSA the slope of the line is much smaller compared to the other sites.**
- **SGP data has better relationship for ΔZ and LWP, but not for cloud temp.**
 - **Derived seasonal relationships?**
- **Azores data has better linear correlation**
 - **Less extreme seasons**
- **Include weighting to account for instrumental error**

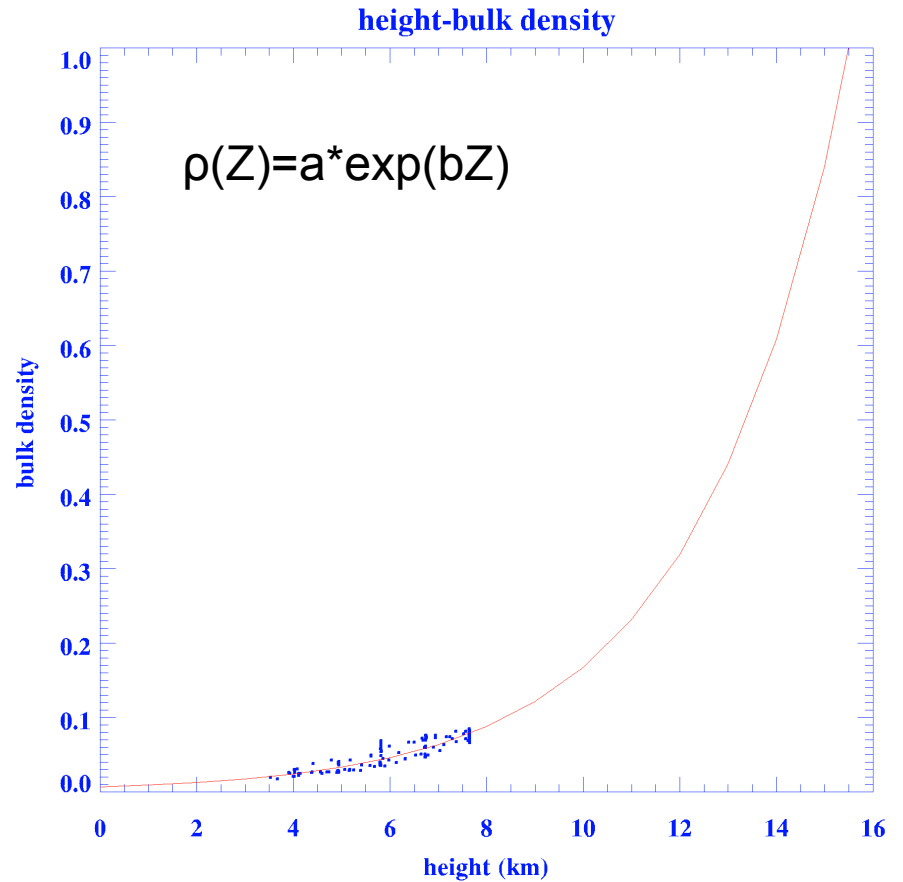
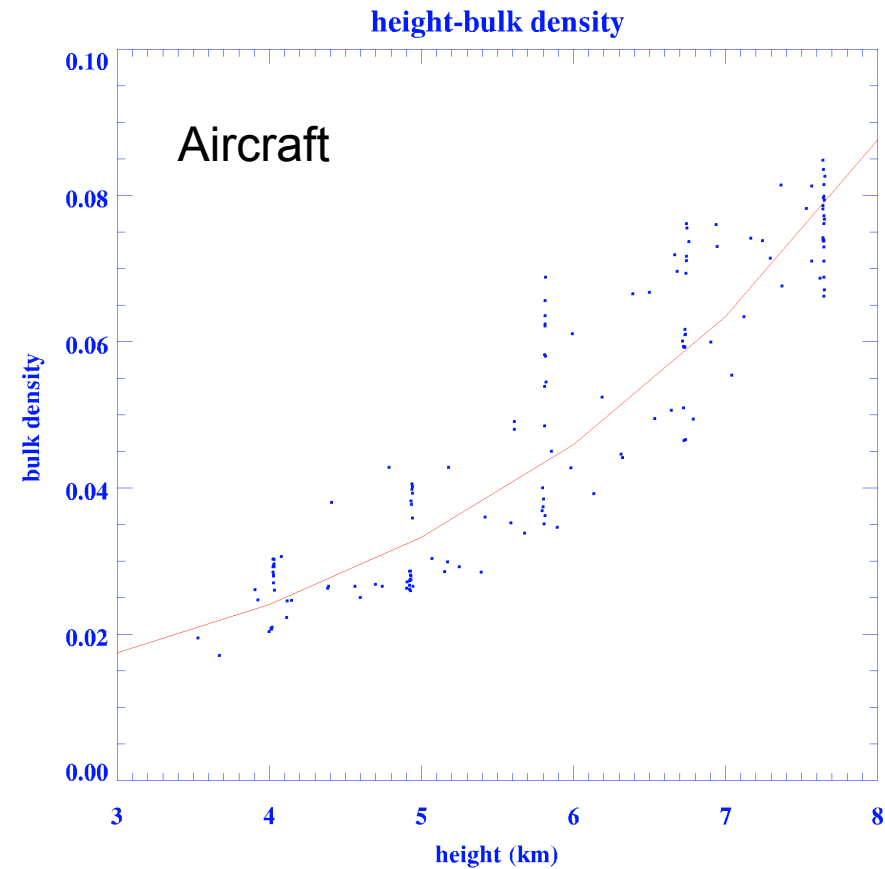
Method 1: assume $\rho=1$ (water)



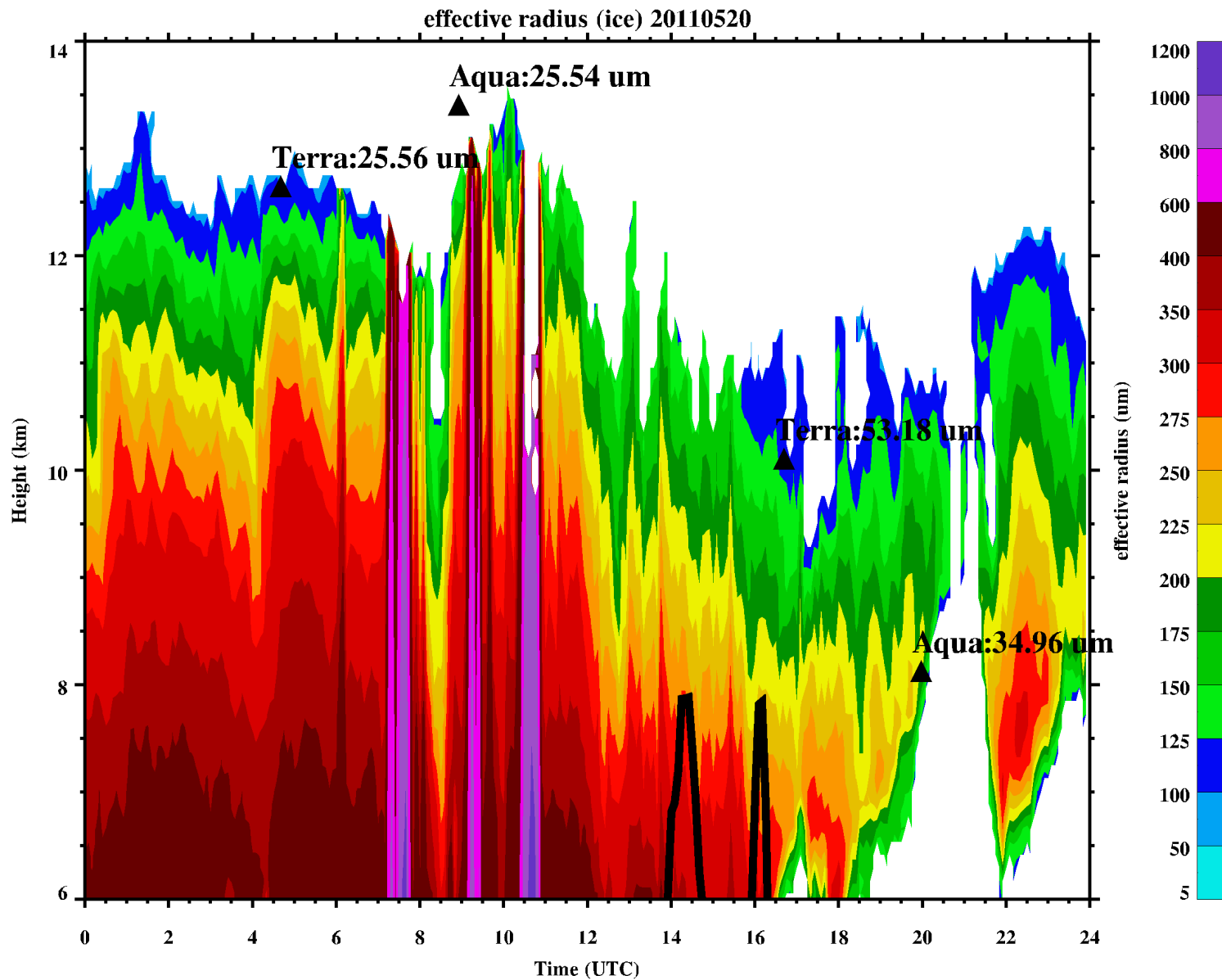
Re at T2 overpass is the most close one to our retrieval, and the other 3 are much smaller than Re retrieved by M1.

30x30km²/100x100km²
IWP(SFC) = 648/1190 gm⁻²
IWP(CERES)=515 /878 gm⁻².

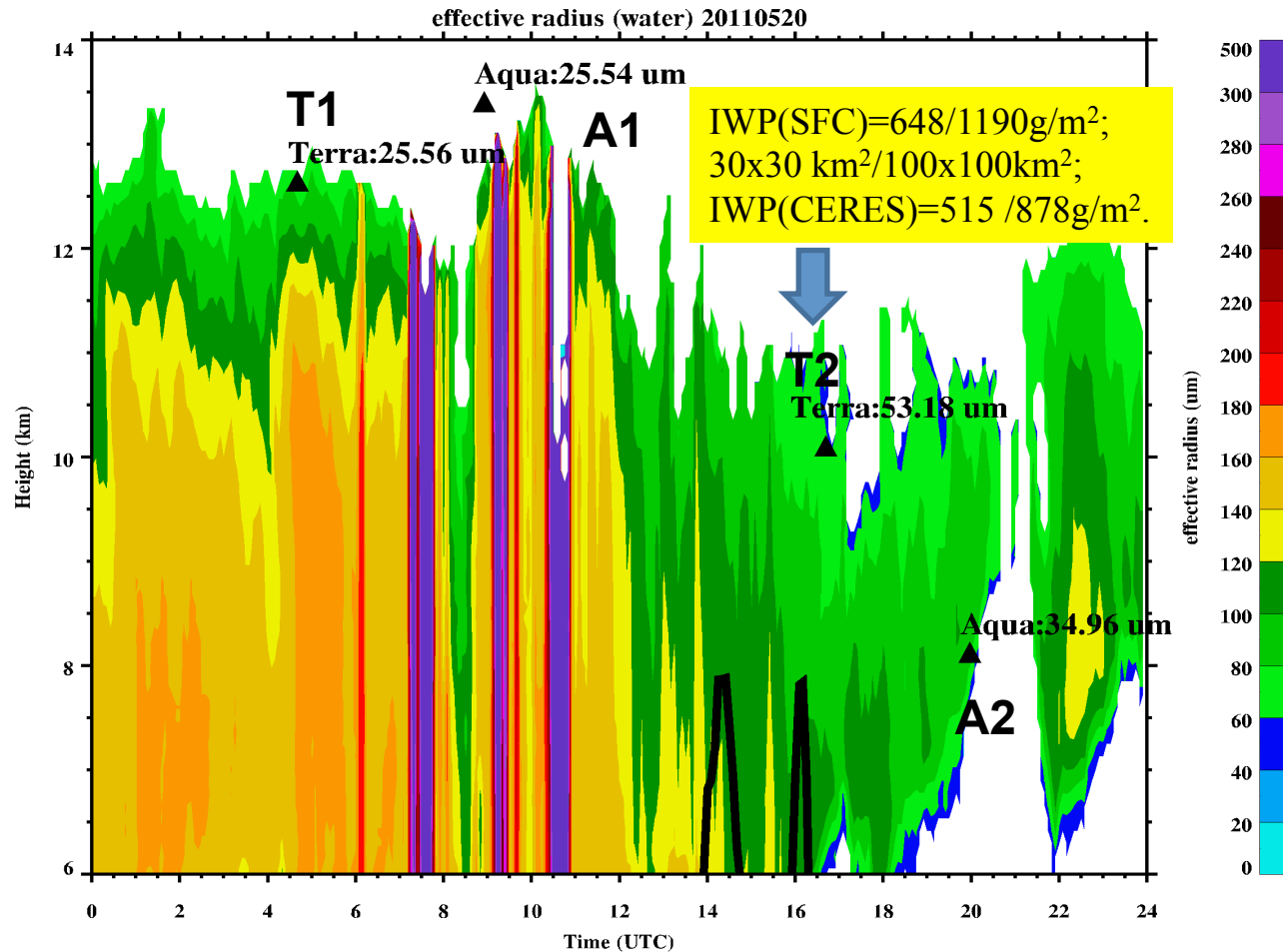
Bulk density: ρ



Re retrieved by Method 2: assume $\rho(Z)=a * \exp(bZ)$

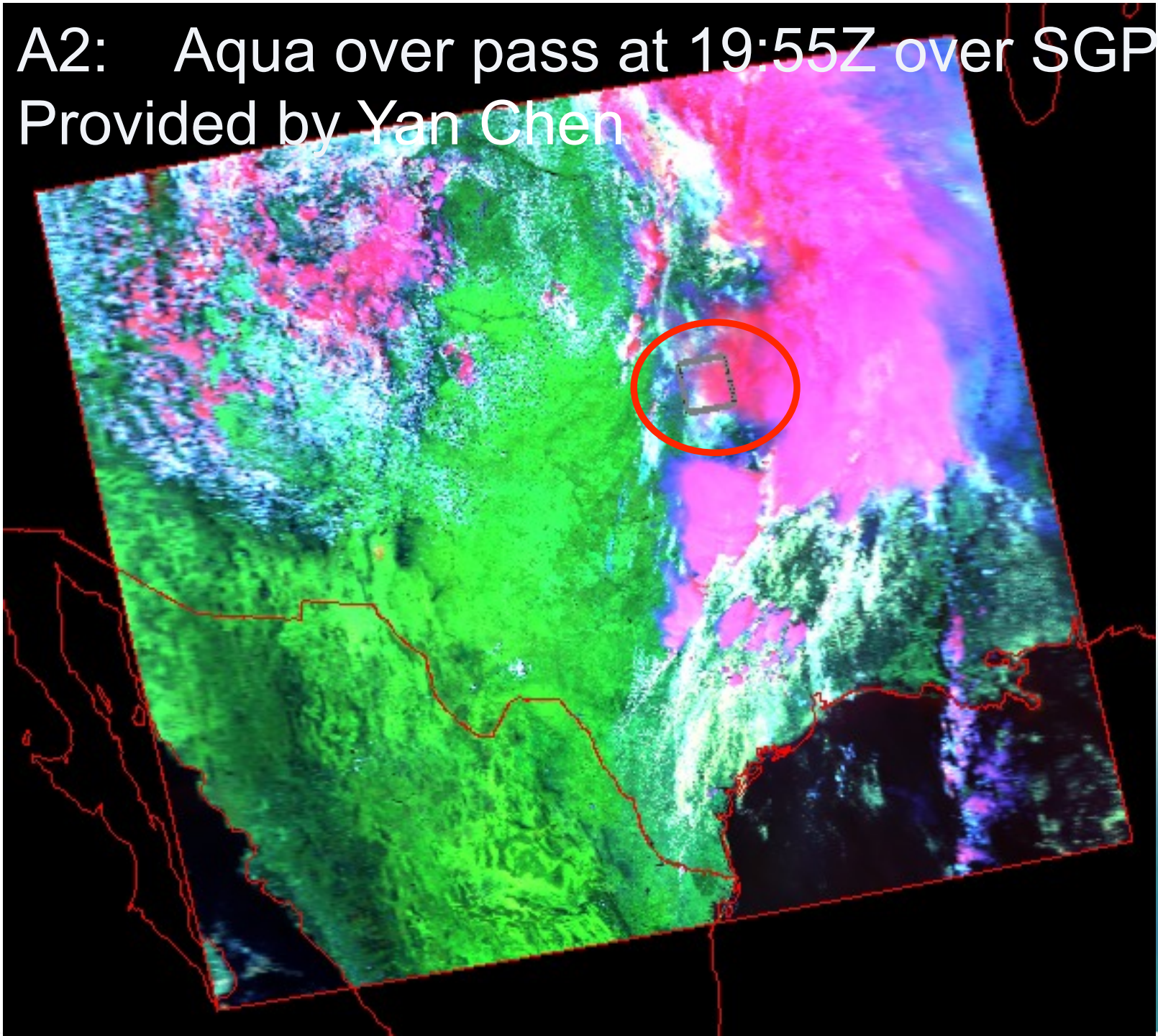


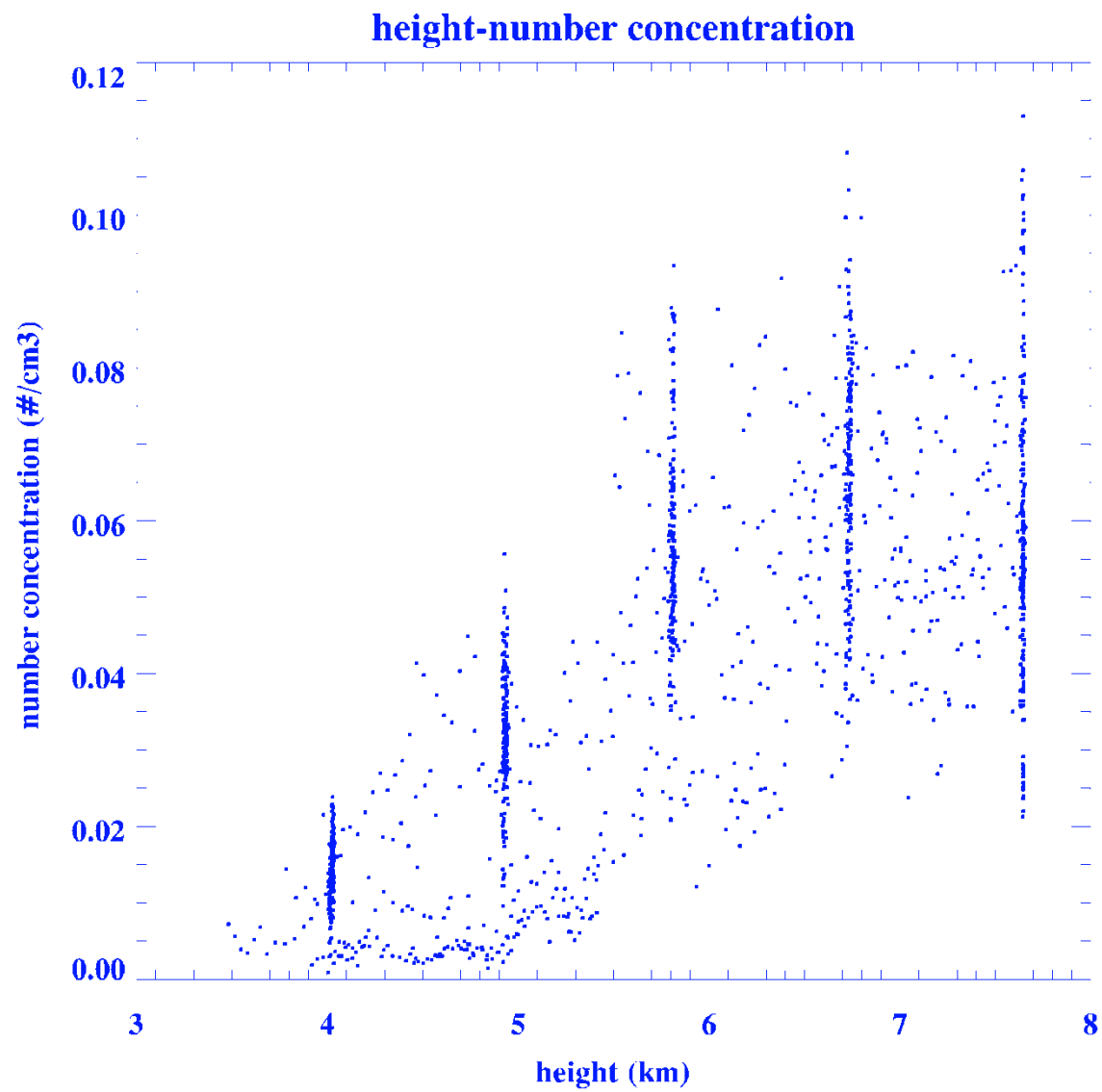
Ice Water Path

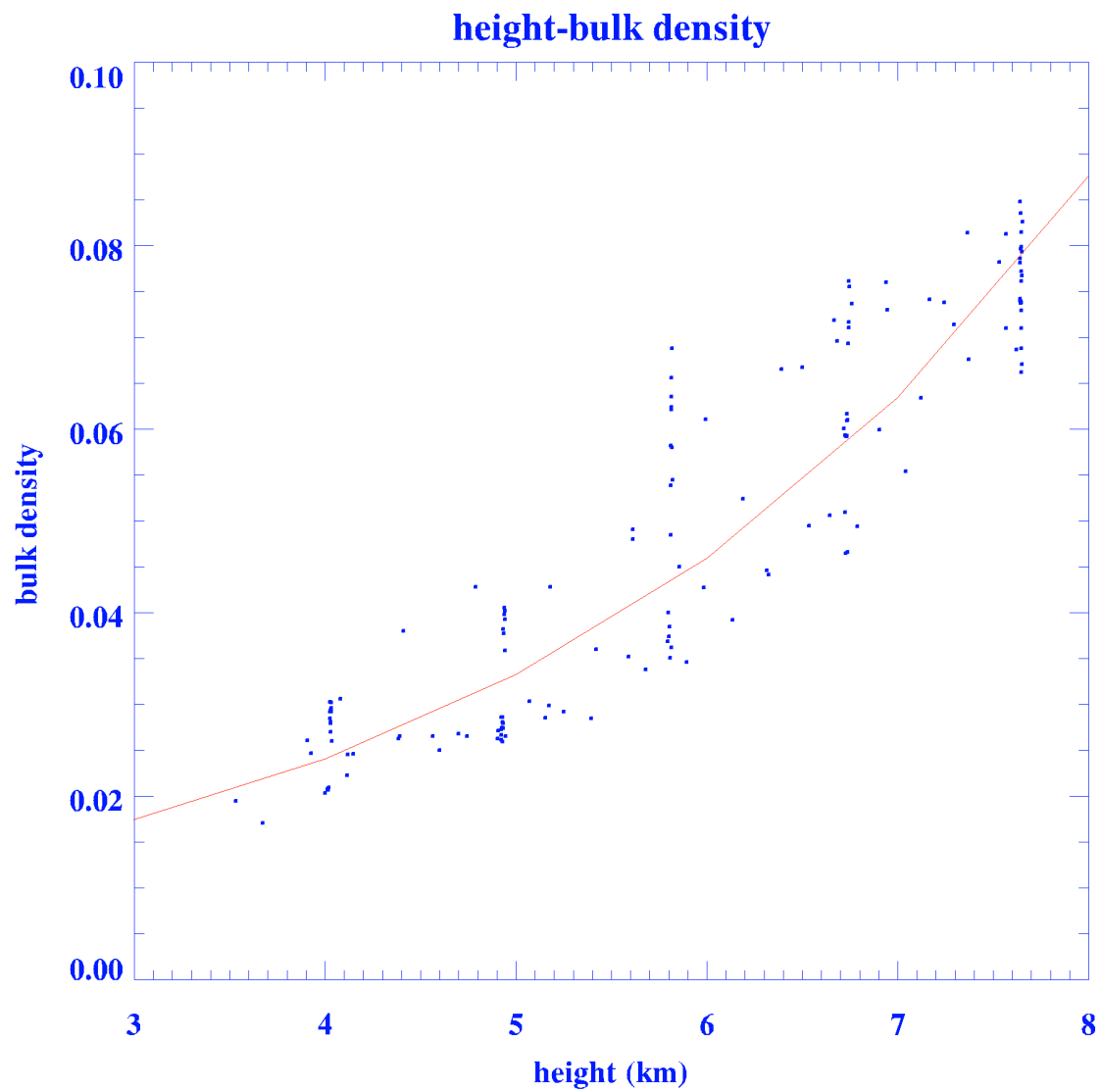


Since there is aircraft measurement (IWC) closed to T2 overpass, we compared the IWP calculated by using aircraft measured IWC and NEXRAD cloud thickness over 30x30 km^2 and 100x100 km^2 centered at SGP

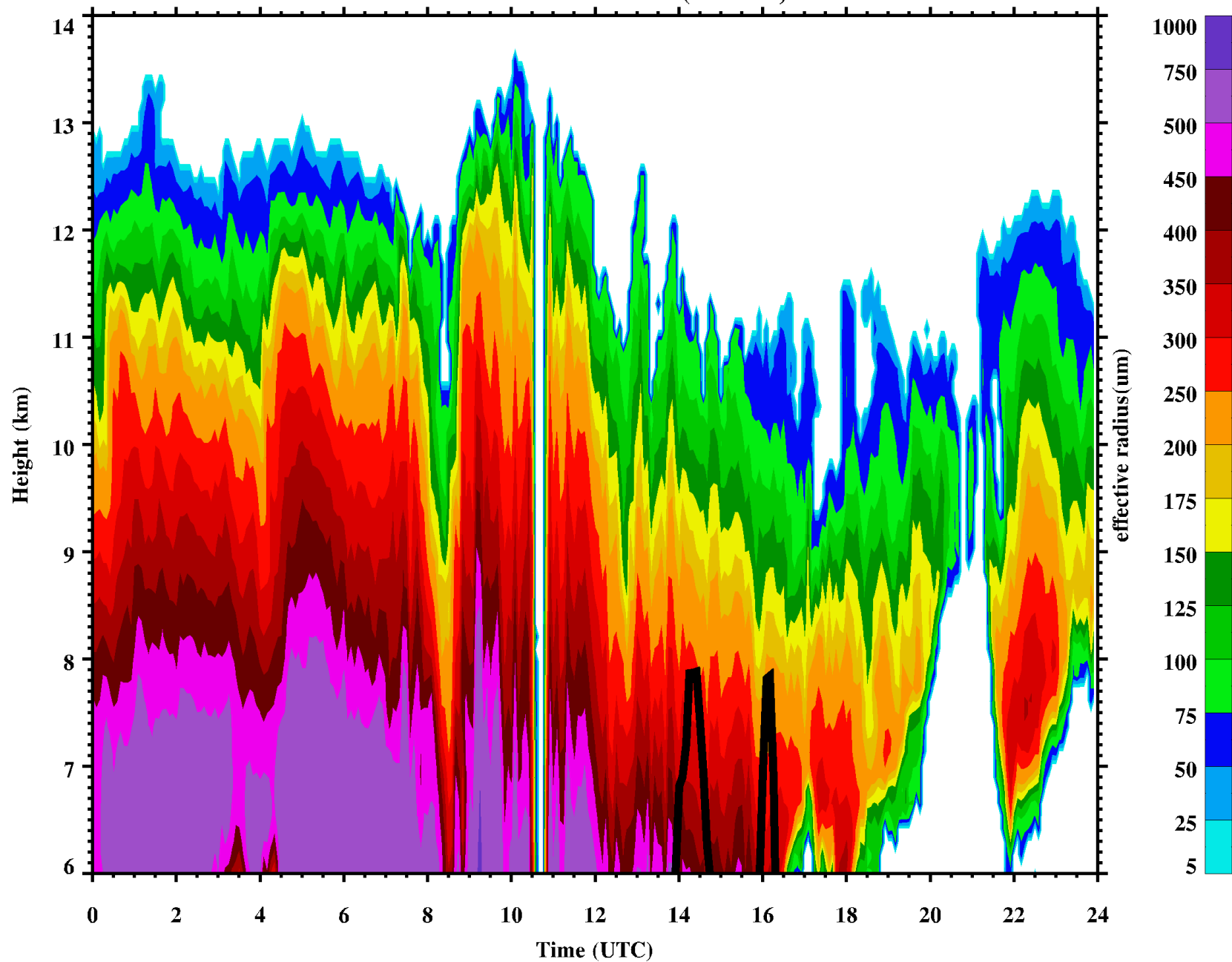
A2: Aqua over pass at 19:55Z over SGP
Provided by Yan Chen



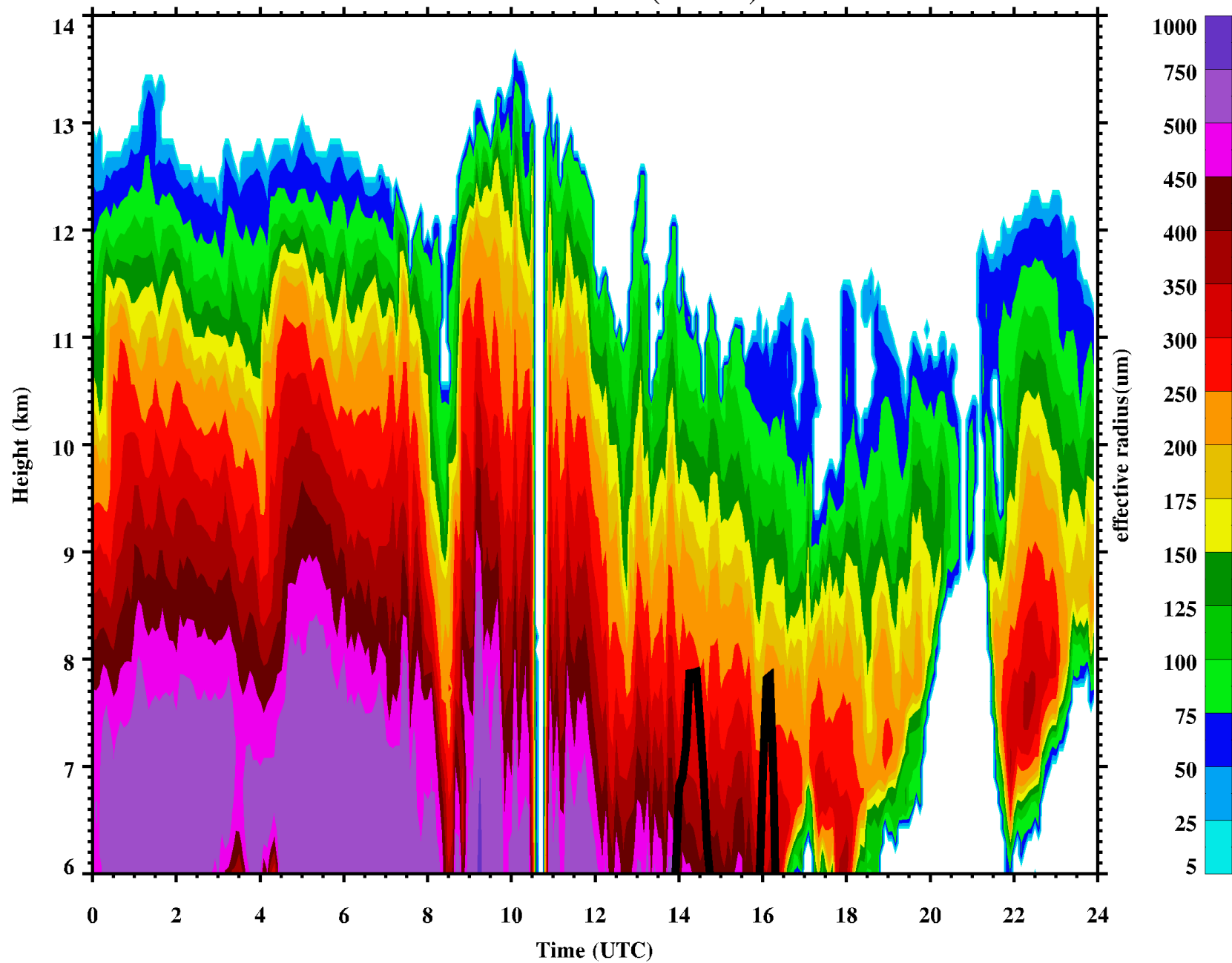




20110520 effective radius (n=0.08) bd



20110520 effective radius (n=0.06) bd+std



Cloud droplet terminal fall speed

TABLE 8.1. Terminal Fall Speed as a Function of Drop Size (equivalent spherical diameter) (From Gunn and Kinzer, 1979)

Diam. (mm)	Fallspeed (m/s)	Diam. (mm)	Fallspeed (m/s)
0.1	0.27	2.6	7.57
0.2	0.72	2.8	7.62
0.3	1.17	3.0	8.06
0.4	1.62	3.2	8.26
0.5	2.06	3.4	8.44
0.6	2.47	3.6	8.60
0.7	2.87	3.8	8.73
0.8	3.27	4.0	8.83
0.9	3.67	4.2	8.93
1.0	4.05	4.4	8.98
1.2	4.61	4.6	9.03
1.4	5.17	4.8	9.07
1.6	5.65	5.0	9.10
1.8	6.09	5.2	9.12
2.0	6.49	5.4	9.14
2.2	6.86	5.6	9.16
2.4	7.27	5.8	9.17

- 1) $0 < r < 40 \text{ } \mu\text{m}$, $V_f = K_1 r^2$, Stokes' law, $K_1 = 1.19 \cdot 10^6 \text{ cm}^{-1} \text{ S}^{-1}$
- 2) $40 < r < 0.6 \text{ mm}$, $V_f = K_2 r$, linear law, $K_2 = 8 \cdot 10^3 \text{ S}^{-1}$
- 3) $0.6 < r < 2 \text{ mm}$, $V_f = K_3 r^{1/2}$, Square root law, $K_3 = 2.2 \cdot 10^3 (\rho/\rho_0)^{1/2} \text{ cm}^{-1} \text{ S}^{-1}$, ρ is air density, ρ_0 is a reference density of 1.2 kg/m^3 . (Rogers and Yau book, P124-126)

how to get z (radar reflectivity factor)

- All the Doppler weather radars provide a measurement of equivalent radar reflectivity factor.
- use drop size distribution, particle size data

$$Z = \int_0^{\infty} N(D) D^6 dD$$

When particle size data are analyzed to determine radar variables, the quantity usually calculated is the radar reflectivity factor Z and not the equivalent radar reflectivity factor Z_e . (Smith, 1984)

equivalent radar reflectivity factor---radar reflectivity factor relationship for ice particles:

For ice particles:

(Atlas ,1995; Smith,1984;Wang 2001)

$$Z_e = \frac{|K|_i^2}{|K|_w^2} Z.$$

From KAZR

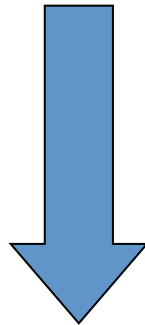
Dielectric factor: 0.88

K_i/ρ_i is nearly constant as particle bulk density changes.

For solid ice, bulk density is about 0.92

g cm^{-3} , and $K_i^2 = 0.176$. (ATLAS, 1995)

$$\left(\frac{K_i}{\rho_i}\right)^2 \approx 0.208.$$



$$K_i^2 = 0.208 * \rho_i^2$$

Cirrus layer microphysical properties derived from surface-based millimeter radar and infrared interferometer data

Gerald G. Mace

Department of Meteorology, University of Utah, Salt Lake City

$$N(D) = N_x \exp(\alpha) \left(\frac{D}{D_x} \right)^\alpha \exp \left[-\frac{D^\alpha}{D_x^\alpha} \right] \quad (2)$$

where D_x is the modal diameter and N_x is the number of particles per unit volume per unit length at the functional maximum. Analysis of in situ data [*Dowling and Radke, 1990*] suggests that for cirrus $\alpha \leq 2$. We therefore set $\alpha=1$ and use observations to estimate D_x and N_x .

$$Z = \int_0^{\infty} N(D) D^6 dD$$

$$N(D) = N_x \exp(\alpha) \left(\frac{D}{D_x} \right)^{\alpha} \exp \left[-\frac{D\alpha}{D_x} \right]$$

$$Z = N_x e^{\alpha} D_x^7 \frac{(6+\alpha)!}{\alpha^{7+\alpha}}$$

$$N_T = D_x N_x e^{\alpha} \frac{\alpha}{\alpha^{\alpha+1}}$$

N_T is the total particle concentration

$$r_e = \frac{D_x}{2} \frac{(3+\alpha)!}{(2+\alpha)!} \alpha^{\alpha}$$

r_e is the effective spherical radius

$$Z = N_T * 2^6 * r_e^6 * \frac{(6+\alpha)!}{\alpha^{6\alpha+7} * (3+\alpha)^6} * 10^{-12} \text{ --- } (mm^6 / m^3)$$